

Crystal structure of ilmenite (FeTiO_3) at high temperature and at high pressure

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Abstract

The structures of two single crystals of synthetic ilmenite were refined using X-ray intensity data collected at 24, 400, 600, 800, and 1050°C (1 atm) and 0.001, 25.4, 34.6, and 46.1 kbar (room temperature). Thermal expansion of the unit cell was nearly isotropic, whereas compression was relatively anisotropic, with c/a decreasing linearly with increasing pressure. The isothermal bulk modulus and its pressure derivative determined from cell volume data are $K_o = 1.70(7)$ Mbar, $K'_o = 8(4)$, or $K_o = 1.77(3)$ if K'_o is assumed to be 4(1). Mean Fe-O and Ti-O distances increased linearly with temperature and decreased linearly with pressure, $\langle \text{Fe}-\text{O} \rangle$ being about twice as expandable and compressible as $\langle \text{Ti}-\text{O} \rangle$. The responses of the two octahedral sites to temperature and pressure were quite different from one another, however. The longer of the two independent Fe-O bonds was more expandable and less compressible than the shorter one, whereas the opposite was true for the Ti site. The Ti atom was displaced toward the centroid of its coordination polyhedron at high temperature, but the Fe atom moved further away from its centroid position. Cation shifts were much smaller with pressure than with temperature. These results indicate that the responses of the ilmenite structure to temperature and pressure are not inverse in character. The cation sites remained fully ordered at all temperatures and pressures studied.

Introduction

Ilmenite (FeTiO_3) occurs as an accessory mineral in a wide variety of igneous and metamorphic rocks (Haggerty, 1976; El Goresy, 1976a,b; Rumble, 1976). One of its most valuable characteristics for petrogenetic studies has been the use of compositions of coexisting hematite-ilmenite and magnetite-ulvöspinel solid solutions as an indicator of temperature and oxygen fugacity at the time of last equilibration (Lindsley, 1963; Buddington and Lindsley, 1964). More recently, other geothermometers have been based upon coexisting ilmenite and olivine or pyroxene (Andersen and Lindsley, 1979; Bishop, 1980) and have utilized solution models to extend the experimental calibrations. The ilmenite structure may also be an important one for metasilicates undergoing high-pressure transformations in the Earth's mantle (e.g., Ringwood, 1969; Liu, 1977a). In order to improve thermochemical models, understand crystal-chemical partitioning behavior, and characterize the pressure-temperature systematics of compounds with the ilmenite structure, it would be

useful to determine the effects of elevated temperature and pressure upon the crystal structure of ilmenite.

The ilmenite structure was determined by Barth and Posnjak (1934). Shirane *et al.* (1959) determined the magnetic structure at low temperature using neutron diffraction, and the structure of lunar ilmenite was studied by Raymond and Wenk (1971). Numerous other investigations have elucidated the magnetic properties of ilmenites and hematite-ilmenite solutions (e.g., Ishikawa, 1958, 1962; Shirane and Ruby, 1962; Shirane *et al.*, 1962; Thorpe *et al.*, 1977) and have suggested the possibility of an order-disorder transformation at high temperatures as is observed for intermediate compositions. Burton (1980) studied such a transformation in an intermediate hematite-ilmenite by single-crystal X-ray diffraction.

Recently, high-pressure structure refinements have been reported for several materials with the closely related corundum structure (Finger and Hazen, 1980). Compression of ilmenite has also previously been studied by X-ray diffraction (Liu *et al.*, 1974) and Mössbauer spectroscopy (Vaughan and Drickamer, 1967) on polycrystalline specimens. A number of other studies have considered the elasticity, crystal-chemical systematics, and high-pressure phase transformations in other compounds possessing the ilmenite structure (Liebermann,

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Ilmenite at 24°C.

L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC					
1	4	L		2	-1	L		3	-3	L		4	-8	L		4	0	L		5	-3	L			
0	9157	9106	614984	14905	9	849	815		3	886	806	1	525	261	14	7838	7931	2	3345	3363					
1	6	L	9	3354	3430	18	6935	6900		4	-7	L		16	2817	2796	5	888	922						
1	968	1000	12	3305	3323	18	3859	3851		3	-2	L		11	496*	155	3	2976	3043						
2	-7	L	5	1859	1830	11	423	444		2	4970	4874	14	9074	9041	6	7299	7354							
3	469*	590	11	1076	1085	20	5580	5550		4	-6	L		15	829	869	3	994	978						
9	553	371		2	1	L		3	-1	L		1	851	925		4	2	L							
2	-6	L	1	2938	2884	13	441*	325		4	6435	6534	7	489	391	2	1507	1469	5	0	L				
5	1515	1485	412093	12423	16	4773	4719		10	8130	8221	14	6508	6552	14	7632	7721	3	436*	180					
8	3821	3728	1011648	11672	19	467	473			4	-5	L		4	3	L		6	1	L					
11	2250	2139		2	2	L		3	0	L		9	2029	2025		4	6255	6325		2	3363	3445			
2	-5	L	15	1915	1943	018126	17977			7	1296	1283													
1	683	774	410070	10244	3	943	950		4	-4	L		5	-7	L		6	-6	L		7	-6	L		
7	747	750		6	5458	5484	9	970	951		5	411*	174	3	817	814	6	4017	3991	7	719	483			
13	488	306	10	6373	6448	7	980	992		11	759	960	9	757	618	9	542*	130	7	-5	L				
2	-4	L		3	-6	L		2	5603	5644	14	6774	6723		5	-6	L		6	-5	L		6	5448	5344
9	1926	1929	18	3585	3597	8	7338	7404		4	-3	L		5	1081	1022	5	1299	1261	9	1037	1190			
2	-3	L		9	466*	176	17	959	784		1	1131	1129	8	3434	3429	8	3761	3647	7	-4	L			
			12	1153	1100			3	2	L		7	1414	1465	11	1693	1712	11	536	311			8	4049	4023
									4	-2	L			5	-5	L		6	-4	L					
2	2859	2963		5	1036	1041	10	7484	7659		6	3899	3853	6	9679	9523	1	1928	1989		7	-3	L		
14	9324	9316	11	5492	5548	5	2111	2051		3	3	L		4	9017	8952	7	1986	2006	1	353	230			
2	-2	L		3	-4	L		11	472	350		4	-1	L		7	828	786	6	-3	L		7	795	731
7	893	665	13	4411	4404	010725	10823		11	2072	2151				14	7819	7809	3	470	338		7	-2	L	
16	410950	11129	13	930	849	6	4369	4385		14	785	565	9	1219	1220	9	558	374	3	1483	1444				
			19	559	73										15	1300	1269								

L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC			
1	1	L		1	4	L		2	1	L		3	0	L		3	3	L		4	1	L		5	1	L
014225	14231	3	2048	2093	411399	11735	017516	17397	6	3124	3205	0	7878	7756	4	5277	5292	10	4814	4815						
3	9046	8921	9	2038	1986	10 9979	10026	6	4709	4718	9	343*	206	6	5688	5754										
612494	12642	15	706	409	16 2348	2284	12 1720	1649	12	694	657	12	582	268												
9	5159	5266			18 4559	4578	15 1015	873				4	2	L												
12	913	930	1	5	L		2	3	L		3	1	L		3	4	L		2	1068	1073	0	4724	4739		
15	1124	1121			18 4218	4275	5	663	612	5 1873	1871	2	4892	5001	5	546	427	8	2823	2692	6	3706	3821			
21	1229	1215	11	1026	1003	11 577*	350	71	8 6353	6334	17 641*	71	11 527	185	14 4959	5029	14 4197	4164					5	3	L	
1	2	L			1	6	L		2	4	L		3	5	L		4	3	L		2	788	388			
5	421	560			5	993	874		3	2	L		1	511*	325	4	4441	4460			6	0	L			
11	2038	2073	7	823	606	1	529	561		7	472*	112	4 8398	8584		4	0	L		10	3996	4038	0	6647	6485	
17	902	881			17	2	0	L	13	498	530	10 5542	5738													
1	3	L			1	2	3104	3168	2	5	L		16 2488	2426	4 7556	7489			5	0	L		6	2918	2724	
1	736	869	8	6192	6140				3	3	L		10 7698	7694	2	1162	941			6	1	L				
7	2024	2069	14	8214	8223	3	875	864	9 555*	72	0 8674	8553	16 1580	1762	8	2480	2433			14 4934	5014	2 2338	2325			
13	1157	1311	20	3473	3365	3	522*	399	3	522*	161									8	3129	3060				

L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC		
1	1	L		1	4	L		2	1	L		3	0	L		3	3	L		4	1	L
013991	14122		3	1734	1811		411122	11413		016934	16969	6	2750	2868	0	7328	7229	4	4674	4747		
3	8882	8699	9	1809	1927		10	9404	9459	6	4426	4504	9	484	388	6	5136	5305	10	4103	4163	
612262	12393		15	623*	304		16	2019	2035	12	1458	1480	12	685	584	12	481	284	5	2	L	
9	5158	5297					18	3952	3913	15	706	688										
12	814	952		1	5	L		2	3	L		3	1	L		3	4	L		0	4198	4154
15	826	891		5	540	482	5	1714	1768	2	4680	4792	5	752	421	2	655	973	6	3295	3267	
18	3618	3701		11	642	761	11	494*	322	8	5968	5942	11	786	227	8	2393	2414				
21	934	782					17	962	219	14	4418	4496				14	3449	3499	5	3	L	
1	2	L		1	6	L		2	4	L		3	2	L		3	5	L		4	3	L
5	326	413		1	676	803	1	475*	435			1	495	233	4	3878	3934	6	0	L		
11	1773	1869		7	585*	413	7	494*	141	4	7867	7978				10	3327	3426				
17	604*	1021		2	0	L	13	552*	648	10	4932	5208	4	0	L				0	5866	5744	
1	3	L					16	2139	2066	16	2139	2066				5	0	L	6	2305	2378	
1	921	867		2	3010	3099	2	5	L		3	3	L		4	7121	7098					
7	1819	1818		8	6010	5958	3	747	886	10	6986	6997	2	660	851	6	1	L				
13	1369	1414		14	7580	7549	9	536*	23	0	7916	7813	16	1507	1557	8	2345	2183	14	4220	4281	
19	761*	505					3	513*	107						8	2806	2575					

L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC	L	OBS	CALC
1	3	L	2	1	L	3	1	L	4	0	L	5	1	L	1	728	817
7	2660	2731	1012030	12043	8	7423	7478	1010036	10058	10	7194	7220	2	412588	12947		
13	875	881	16	3396	3386	14	7014	7082	16	2814	2818	5	2	L	19	604*	75
1	4	L	2	3	L	3	2	L	4	1	L	0	6864	6877	3	2848	2926
9	2018	2039	17	953	811	16	3959	3911	12	537*	325	6	5805	5753	5	1973	2058
15	585*	787	2	4	L	3	3	L	4	2	L	0	9186	9106	1	5	L
5	940	1009	1	880	955	011099	11039	2	1506	1476	6	4058	4105	7	523*	413	
11	1689	1764	13	635	110	3	481	579	8	3802	3758	6	1	L	1	6	L
1	6	L	2	5	L	12	1013	1077	14	6531	6591	2	3384	3457	1	1023	982
7	1452	1350	3	766	767	15	1175	1176	4	6372	6373	1	3210	3373	9	719	599
2	0	L	3	0	L	5	336*	517	5	0	L	8	6592	6621	1	10511	12284
1410585	10511	12284	6	5511	5541	3	5	L	2	1461	1268	18	6973	6910	14	7858	7790
20	5482	5421	1	647	719	3	4	L	3	3248	3240	1	140585	10511	1	6973	6910

Ilmenite at 34.6 kbar

"Values given are 100 times the observed and calculated structure factor amplitudes. Those marked with an asterisk are considered below the minimum observable and were excluded from structure refinements."

Ilmenite at 46.1 kbar.

OBS	CALC	H	OBS	CALC	H	OBS	CALC	H	OBS	CALC	H	OBS	CALC	H	OBS	CALC	
H -9 2		H -6 -1			H -4 -2			H 1 -6			H 3 -2			H 5 -3			
552* 689	2	612*	1180		6 1542	1436		4 7864	7788		-8 1109	1002		-7 1262	1208		
H -9 3		H -6 0			H -3 -4			H 1 -5			H 3 -1			-4 2815	2850		
712 159		0 8671	8716		510065	10065		2 2124	2253		-7 737	222		-1 2940	2969		
H -8 0		310479	10566											2 1281	1355	H 7 -3	
9 5560	5569				H -3 -2			H 1 -4			H 4 -6					-5 779	759
5979 5853		H -6 4			1 4805	4692		-314175	13972		1 7890	7980		-2 819	565		
5031 5025		-2 894*	5564		7 3642	3606		6 4351	4317					1 341*	205		
H -8 1		H -6 5			H -3 -1			H 1 -3			H 4 -5			-8 1654	1585		
549* 615		-1 646*	837		-4 540*	338		7 401*	538		2 951	997		-5 1857	1858		
H -8 2		H -5 -4			H -3 0			H 1 -1			H 4 -4			1 870	804	H 7 -1	
818 681		6 6877	7020		317600	17756		0 957	929		3 4668	4699		-6 817	869		
H -8 4		H -5 -3			H -2 -4			H 2 -4			H 4 -3			-3 794	338		
145 5617		7 323*	565		6 6448	6465		4 8451	8412		-5 1180	1180		0 395*	95		
H -7 -2		H -5 -2			H -2 -2			H 2 -2			1 968	1020		-3 4113	4195		
250 2289											4 782	465		0 3719	3871	H 8 -5	
287 1360		-1 1266	1218		-1 2927	2925		6 1193	1030		H 6 -5			-5 1373	1309		
H -7 0		5 1237	1257		8 926	810					1 773	837		-1 773	837	-5 5837	5777
		8 517*	681		H -2 0			H 3 -6			H 6 -3					H 8 -3	
553 6542		H -5 -1			114129	13936		3 4118	4210		H 4 -2			-6 470*	497		
874 6839								H 3 -5			1 1236	1180		-3 302*	499		
550 5557		9 389*	395								3 319*	222		0 522*	153		
I -7 1		H -5 0			7 6309	6285		-5 342*	260		H 5 -6			3 527*	264		
722 95		1 9096	9192		H 0 -4			-2 888	896							H 8 -1	
		4 8856	8961					4 378*	227		-4 7570	7400		-6 401*	429		
I -7 5		5 8737	8712								-1 6965	7169		-3 1036	1050		
599 562		H -5 5						H 3 -4			2 4887	4888		-5 789	615		
I -6 -2														-2 415*	265		
139 1905		-3 583*	571		1 6754	6907		-112176	12300		H 5 -5						
14 3168		H -4 -4			7 2548	2630		2 9675	9648					-1 1513	1507		
98 3217		7 6040	6044		H 0 0			5 6080	5930					2 1505	1387	H 9 -3	
								H 3 -3									
														-6 752	153	H 9 -2	
								-3 1136	1150		H 5 -4						
								0 985	984					-4 449*	493		
								3 323*	416					-1 402*	562		
								6 340*	178		1 8021	8030					